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(54) **Thermotropic liquid crystal polymer composition and insulator**

Thermotrope Flüssigkristallpolymerzusammensetzung sowie Isolator

Composition de polymère thermotrope cristal liquide et isolant

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## Description

This invention relates to a thermotropic liquid crystal polymer (referred to as LCP) composition and, more particularly, to an electrical insulator which, when injection molded, is suitable for use in the structure of electric machines and appliances.

It has been common practice to reinforce liquid crystal polymers with fillers but the filler loading has typically been up to 30 - 40 wt% and it has not been known to improve the insulating and heat conducting properties of the polymers by loading them with fillers through injection molding.

The EP-A-0 423 510 discloses a thermoplastic molding composition which comprises a resin such as polyethylene terephthalate and co-polymers thereof and liquid crystal polymers; and from 20 to 85 wt.-% of the total composition of a filler, which filler may be a zirconium silicate. For certain applications, 60 to 85 wt.-% of the filler component may be employed.

Magnetic iron cores in the stators of small motors, stator coils mounted on the cores and their terminals are exposed to various adverse conditions during practical use such as mechanical stresses due to the pulsating torque and heat generation that accompany motor operation, as well as moisture, water, corrosive atmosphere, corrosive liquids and heat dissipation and, hence, studies have been made to develop effective methods for securing and insulating those members.

A common method adopted to this end comprises insulating stator coils with insulating varnish while securing them to a stator's magnetic iron core using an adhesive, then providing a housing using cast metal parts. However, this method involves not only many steps of manufacture but also much time and materials, thereby increasing the cost of the product. Furthermore, heat and cold cycles and mechanical vibrations that are produced during the operation of rotating machines have frequently caused debonding or deterioration in the insulating performance. These defects are particularly marked in motors that are caused to run at high speed at high frequency on a variable frequency power supply, as by PWM inverter control (e.g. variable voltage, variable frequency control, generally referred to as "VVVF control").

With a view to solving the problem, a method has been proposed that performs resin molding on the stator iron core and coils as a whole. The resin composition that is to be used in this method and which is capable of monolithic molding is required to meet the following requirements. First, the resin composition must exhibit very good adhesion to the stator's magnetic iron core and coil. Second, it must retain its insulating quality for a prolonged time while enhancing the dissipation of heat generated during the operation of a rotating machine and yet without causing debonding. Third, it is required that heat and cold cycles due to the start and stop of the rotor or the vibrations that occur during operation should not develop cracks in the molding layer to deteriorate the insulating performance or dimensional precision of the machine, thereby insuring that the rotor will turn smoothly. Fourthly, electromagnetic considerations for rotating machines require that the many slots in the stator's magnetic iron core should be completely filled with the resin to avoid any disturbances in the distribution of electric lines of force while, at the same time, the pulsating vibrations that occur during the operation of the rotating machine should not cause the resin to separate from the core, develop cracks or break into pieces that collide against the rotor.

Most importantly, the resin composition must have good insulating quality among other things. Once molding is accomplished, retouching is no longer possible and, hence, absolute reliability is required for the characteristics of the resin composition.

For resin molding of conventional electric machines and appliances, liquid unsaturated polyester resins, vinyl ester resins and epoxy resins have been used by means of cast molding, low-pressure molding or vacuum cast molding, but this method has caused the following problems in terms of manufacture and performance: (1) long curing time; (2) the filler is precipitated during curing to form a resin-rich portion and, hence, cracking is prone to occur on account of heat cycles; (3) the shaped part must be enclosed with a casing (container) and this makes it difficult to produce complexly shaped parts; (4) air voids are prone to occur in the shaped part but they are not desirable from the viewpoint of performance; and (5) the part being cured is highly susceptible to the effect of atmospheric moisture. In short, cracking will occur during resin molding by the prior art technique on account of various factors including shrinkage upon curing, heat cycles, air voids and the difference in the degree of curing, and this has made the occurrence of time-dependent deterioration unavoidable.

It has generally been held that solving all of the aforementioned problems of the prior art is extremely difficult. An injection molding technique that is capable of high filler loading and high production rate is useful as a means for solving the problems but injection molding materials so far available have defied injection molding since they are liquid resins which involve chemical reaction.

The present invention has been accomplished under these circumstances and has as the general object providing an injection molding material that is free from the afore-mentioned problems of the prior art. Stated more specifically, it is an object of the present invention to provide a thermotropic LCP composition that is improved in handling property and adaptability for mass production and which has high insulating, heat conducting, thermal expansion and reliability

characteristics.

It is another object of the present invention to provide an electrical insulator having the same features as mentioned just above.

It is still another object of the present invention to provide a stator that is resin-molded using said electrical insulator.

Other objects and advantages of the present invention will become apparent to those skilled in the art from the following description and disclosure.

Fig. 1 is a sectional view of a submersible canned motor according to the present invention;

Fig. 2 is a sectional view of the stator of submersible motor according to the present invention;

Fig. 3 is a sectional view showing an illustrative mold structure that is to be filled for injection molding;

Fig. 4 is a cross section of Fig. 3 as taken on line A-A';

Fig. 5 is a sectional view showing another illustrative mold structure that is to be filled for injection molding;

Fig. 6 is a sectional view of a resin-molded motor according to the present invention;

Fig. 7 is a sectional view showing details of a part of the stator core and resin-molded can that are shown in Fig. 6; and

Fig. 8 is a sectional view showing another example of the resin-molded motor according to the present invention.

The first object can be attained by a thermotropic LCP composition according to claim 1.

The second object can be attained by an electrical insulator according to claim 3.

The third object can be attained by a resin-molded stator for electric machines or appliances according to claim 5.

The stator of the present invention not only insures good electrical insulation but also has an expansion coefficient very close to those of metals; hence, it is free from any debonding and cracking, thus claiming high reliability.

In accordance with the present invention, a thermotropic LCP that has an inorganic mineral filler of high heat conductivity blended homogeneously is injection molded and this enables the production of a resin molded electric machine or appliance that is not only free from all defects of the prior art but which is also furnished with new capabilities such as vibration damping characteristics and barrier quality against corrosive gases. Furthermore, the adoption of injection molding process doubles or even triples the production rate of the prior art.

The thermotropic LCP resin as used in the present invention is a thermoplastic aromatic polyester. According to the differences in basic molecular structure, thermotropic LCPs are currently available in three types and they vary greatly in heat resistance. While all types are copolymers of polyester types containing parahydroxybenzoic acid (PHB), type 1 is a copolymer of terephthalic acid (TA) and p,p'-biphenol (BP) with a heat distortion temperature (HDT) or deflection temperature under load of 275 - 350°C; type 2 is chiefly composed of 2-oxy-6-naphtoic acid (2,6-NA) with HDT of 180 - 240°C; and type 3 is a copolymer of PHB and PET (polyethylene terephthalate) with HDT of 64 - 210°C. Each type has a low melt index and high fluidity, exhibiting high dimensional stability due to low linear expansion coefficient, small shrinkage upon molding and small dimensional changes upon moisture absorption, as well as good vibration damping characteristics, high strength and high elastic modulus; at the same time, the three types of the thermotropic LCP resin have the high electrical strength and arc resistance that are necessary for use with electric machines and appliances.

High-molecular weight materials are generally poor in heat conduction and, in particular, thermotropic LCPs have great anisotropy under the influence of crystal orientation during molding and their weld strength tends to decrease. Hence, a large amount of inorganic mineral filler is used in the present invention with a view to achieving improvements in that nature of thermotropic LCPs. To attain the primary purpose of not deteriorating electrical characteristics and for the secondary purpose of filling small gaps such as the spaces between turns of the stator coil with the thermotropic LCP, the fine particles of zircon having the structural formula  $ZrSiO_4$ , such as zircon sand (zircon flour; 350 mesh pass  $\geq 96.5\%$ ;  $\leq 60 \mu m$ ) may be used as an inorganic mineral.

Zircon flour is used in an amount of 90% to more than 85% by weight of the thermotropic LCP, and the two ingredients are mixed under heating at a temperature of 260 - 330°C to form pellets (grains) having a homogeneous composition. Besides zircon, various inorganic mineral fillers may be mixed with the thermotropic LCP in the present invention in an amount of up to 40% by volume of zircon and they include: silica, clay, talc, asbestos, kaolin, dolomite, chromite, alumina, mica, magnesite, titanium oxide, beryllium oxide, magnesium oxide, calcium oxide, slate, chalk, silica sand, Shirasu (mixture of volcanic ash and pumice produced in a southern region of Kyushu, Japan), mountain sand, river sand, fused quartz, glass powder, and other various materials prepared by processing naturally occurring inorganic substances into a powder form. The amount of addition of these inorganic mineral fillers may be expressed in terms of weight ratio as determined by calculation on the basis of the specific gravity of zircon.

The amount of addition of zircon is specified to be more than 85% by weight in the present invention because below this amount, the heat conductivity that can be attained is too low to justify the addition of zircon. If zircon is added in amounts exceeding 90%, the mixer and pelletizer and, even the injection molding machine and the mold may wear rapidly or may be subjected to excessive load, thus making it substantially impossible to perform the intended mixing

operation; furthermore, voids will occur in the shaped part of the polymer composition to cause deterioration in its characteristics.

Containing zircon in a large amount, the thermotropic LCP composition of the present invention is an inexpensive and strong electrical insulator that is excellent in electrically insulating, heat conducting and heat resisting properties. By performing monolithic molding with this insulator, electrical insulation and the formation of a housing can be accomplished simultaneously to produce a stator that has good electrical insulation performance, that is small and lightweight and that insures high reliability.

The injection molding pressure is generally in the range of 39.24 - 137.34 MPa (400 - 1,400 kgf/cm<sup>2</sup>), but it varies depending on the shape of the molding. When injection molding is to be performed in two stages, the injection pressure is generally at 58.86 - 137.34 MPa (600 - 1,400 kgf/cm<sup>2</sup>) for the first stage, and at 39.34 - 68.67 MPa (400 - 700 kgf/cm<sup>2</sup>) for the second stage.

The two-step injection molding may be performed in the following manner. In the first stage of injection molding, the slots in the stator core and the space around the coil end portions at opposite ends of the core are filled with a resin composition at a pressure of 58.86 - 137.34 MPa (600 - 1400 kgf/cm<sup>2</sup>). In the second stage, a can, a frame and frame side plates are mounted on the thus produced stator core to form a submersible motor and the resulting space around the coil end portions is filled with a resin composition at a pressure of 39.34 - 68.67 MPa (400 - 700 kgf/cm<sup>2</sup>). If desired, the stator made in the first stage may be used as part of a submersible motor without filling with the resin composition in the second stage.

The following examples are provided for the purpose of further illustrating the present invention but are in no way to be taken as limiting.

#### Example 1

Thermotropic LCP of type 3 (HDT: 170°C) composed of a copolymer of parahydroxybenzoic acid and polyethylene terephthalate was mixed with 85.3% by weight of zircon flour (350 mesh pass  $\geq 96.5\%$ ;  $\leq 60 \mu\text{m}$ ) at a temperature of 270 - 280°C to produce a thermotropic LCP composition of the present invention. The zircon flour consisted of 66 wt% zirconia (ZrO<sub>2</sub>) and 33 wt% silicon dioxide.

The thermal conductivity and linear thermal expansion coefficient of this thermotropic LCP composition were as shown in Table 1, which also show the data for a material (comparison 1) composed of bisphenol A type epoxy resin and zircon sand (86.8 wt%, very coarse as the peak of particle size distribution being 105 - 125  $\mu\text{m}$ ), a material (comparison 2) composed of fibrous glass reinforced plastics (unsaturated polyester and glass fiber: GF content: 30 wt%), a material (comparison 3) composed of polyamide 66 and glass fiber (GF content: 30 wt%), and a material (comparison 4) composed of thermotropic LCP and glass fiber (GF content: 30 wt%).

Table 1

Run	Thermal conductivity (Cal/cm-sec. °C)	Linear thermal expansion ( $\times 10^{-5}/^{\circ}\text{C}$ )
Ex. 1	0.0055	1.97
Comp. Ex. 1	0.0040	2.5
" 2	0.0007	3.0
" 3	0.0006	2.5
" 4	0.0006	2.2

#### Example 2

Additional thermotropic LCP compositions were prepared from a thermotropic LCP and zircon flour as in Example 1, except that the zircon flour content was varied at 45, 60, 70, 85, 90 and 95% by weight. The thermal conductivities and insulation breakdown voltages of the samples were measured and the results are shown in Table 2 together with the data for the inherent values (0 and 100% zircon).

Table 2

Zircon flour content (wt%)	Thermal conductivity (Cal/cm-sec. °C)	Insulation breakdown voltage (kV/mm)
0	0.00033	20.1
45	0.00091	20.3
60	0.00157	20.5
70	0.00251	20.7

Table 2 (continued)

Zircon flour content (wt%)	Thermal conductivity (Cal/cm-sec- °C)	Insulation breakdown voltage (kV/mm)
85	0.0055	20.9
90	0.0072	21.2
95	0.0058	13.9
100	0.0040	NA because of powder

As Tables 1 and 2 show, the samples of the present invention were high in thermal conductivity and insulation breakdown voltage but low in linear thermal expansion coefficient. It can also be seen that the higher the content of zircon flour, the higher the thermal conductivity. Table 2 shows in particular that when the content of zircon flour exceeded 90% by weight, voids occurred in the shaped part of thermotropic LCP composition, causing gradual deterioration in characteristics.

#### Reference Example

A submersible canned motor was fabricated using a thermotropic LCP composition of the present invention and a temperature test was conducted in order to check for improvement in heat conduction. The results are shown in Table 3. The stator could be cooled very efficiently on account of improved heat conduction and heat dissipation from the coil ends was particularly good to provide a uniform temperature profile throughout the motor.

Table 3

Filled materials	Increase in coil temperature (by resistance method) deg C	Increase in coil end temperature (by thermocouple method) deg C	Temperature of cooling water (by thermocouple method) °C
*Thermotropic LCP composition (Reference material)	35.5	46.5	20.5
**Epoxy resin composition (Comparison 5)	48.5	80.0	20.5
*** Air composition (Comparison 6)	66.2	112.5	20.5

\* Thermotropic LCP composition is composed of mixture of 15 wt% of a thermotropic liquid crystal polymer resin and 85 wt% of zircon.

\*\* Epoxy resin composition is composed of mixture of 15 wt% of an epoxy resin and 85 wt% of silica sand.

\*\*\* Air composition is composed of mixture of 60 vol% of air and 40 vol% of an inert dry gas (He gas).

A section of the submersible canned motor is shown in Fig. 1, in which numeral 1 denotes the shaft of the motor, 2 is the rotor fitted on the shaft 1, 3 is the bearing, 4 is the bracket supporting the shaft 1 via the bearing 3, 5 is the stator can isolating a stator compartment 6 from a rotor compartment 7, 8 is the stator core, 9 is electrical insulating paper, 10 is a coil, 11 is the frame in which the stator core 8 is fitted, 14 is the side plate of the frame, and 15 is a lead wire.

The stator compartment 6 is filled for molding with the thermotropic LCP composition of the present invention which is composed of a thermotropic LCP resin and a zircon flour, and the rotor compartment 7 is filled with an aqueous solution of propylene glycol.

Shown by 31 is a sand slinger, 32 is an oil seal mechanism for preventing dust and foul water from entering the rotor compartment, 33 is thrust carbon, 34 is a thrust pad, 35 is a centering ball, 36 is a thrust disk, and 37 is a thrust housing or a thrust bearing mechanism which bears, via shaft 1, the hydraulic axial thrust force that develops when a pump connected to the submersible canned motor under consideration is operated.

Table 3 also shows data for Comparison 5 which had the stator compartment 6 filled with a mixture of epoxy resin and silica, as well as data for Comparison 6 which had the stator compartment 6 filled with a mixture of air and an inert dry gas (He gas).

#### Example 3

In this example, a method is described that enables the stator compartment of a submersible motor to be filled

with the molding material of the present invention which has high electrical insulating and heat conducting properties.

Fig. 2 shows a section of the stator of a submersible motor. Shown by 8 is a silicon steel sheet forming the stator core and the necessary number of such steel sheets are laminated to provide a rated motor capacity and fixed within a frame 11 in predetermined position. Disposed between adjacent steel sheets is a coil 10 protected by a suitable means such as electrical insulating paper, thus forming coil ends 10a and 10b at the respective terminals.

The stator formed a closed compartment by means of a frame side plate 14a on load side, frame side plate 14b on opposite side, and can 5. Both coil ends 10a and 10b were filled with the molding material of the present invention which was injected through gates provided at the respective side plates 14a and 14b.

Figs. 3 and 5 show examples of a mold structure for filling the stator compartment of the submersible motor shown in Fig. 2 with the molding material in Example 1 of the present invention by injection molding. Fig. 4 shows a cross section of Fig. 3 as taken on line A-A'. Figs. 3 and 4 show a mold for primary injection molding, by means of which gaps can be filled completely without causing damage to the windings of coil 10 arranged in slots 19 in a stator core 8, as well as coil ends 10a and 10b at both terminals of the coil. Fig. 5 shows a mold for secondary injection molding. After primary injection molding, can 5, frame 11 and frame side plates 14a and 14b are mounted on the produced stator core to form a submersible motor and the resulting space around the coil end portions is filled by the secondary injection molding.

In the primary injection molding, a stator core with the coil windings placed in slots is set in the mold and the resin of the present invention is injected at high pressure for filling the mold via a sprue 24 and gate 29 provided in the hollow portion of the stator core. Since the filling resin material is to flow by large length, the injection pressure was appropriately in the range of 78.48 - 117.72 MPa (800 - 1200 kgf/cm<sup>2</sup>) in Example 3.

The mold for secondary injection is shown more specifically in Fig. 5. The mold is divided by line X-X into two parts, a fixed part 22 and a movable part 23, each being furnished with a temperature control circuit 28 for adjusting the mold temperature. Stator 21 is reinforced with jigs 26a, 26b and 26c for preventing deformation of the stator and lifted by a hoist 27 so that it is set properly in the movable part 23.

With the stator 21 set in proper position, the molding material is injected through the sprue 24 for molding. Thereafter, the mold is opened at parting line X-X and ejector plate 25 is actuated so that the stator 21 is extracted from the movable part 23 together with reinforcements 26a, 26b and 26c and recovered by means of the hoist 27.

This procedure completes the process of filling one of the two coil ends 10a and 10b and, by repeating the same procedure, the other coil end can be filled for molding. In the secondary injection molding, the cavity to be filled has a large mass (capacity) but the molding polymer composition need to flow by a short length, so an injection pressure of 49.05 MPa (500 kgf/cm<sup>2</sup>) is sufficient to effect the necessary filling of the mold.

#### Example 4

Fig. 6 shows a section of a motor that is resin molded in accordance with the present invention. Shown by 1 is the shaft of the motor, 2 is a rotor fitted on the shaft 1, 3a and 3b are bearings, 4a and 4b are brackets that support the shaft 1 via the bearings 3a and 3b, 17a and 17b are resin molded cans that isolates a resin molding portion 18 from rotor compartments 7a and 7b and which are formed as an integral part of the resin molding portion 18 without creating any borderline, 8 is a stator core, 9 is insulating paper, 10 is a coil, 18 is the resin molding portion which serves as a housing in which the stator core 8, coil 10 and electrical insulating paper 9 are confined forming an integral assembly (the stator compartment 6 shown in Fig. 1 is included within this portion), and 15 is a lead wire. The rotor compartments 7a and 7b are either vacuum or filled with a fluid (gas or liquid).

Fig. 7 is a sectional view showing details of part of the stator core 8 and resin molded can 17 which are shown in Fig. 6. Shown by 8 is the stator core, 17 is the resin molded can, 9 is electrical insulating paper, 10 is the coil and 16 is a wedge. These members are confined forming an integral assembly within the resin molding portion 18 which serves as a housing. The resin molding portion 18 also serves as stator can 17 in the area where the stator core 8 faces the rotor 2, thereby achieving isolation from the rotor compartment 7.

#### Example 5

Fig. 8 is a sectional view showing another motor that is resin molded in accordance with the present invention. Shown by 1 is the shaft of the canned motor, 2 is a rotor fitted on the shaft 1, 3a and 3b are bearings, 4a and 4b are brackets that support the shaft 1 via bearings 3a and 3b, 5 is a stator can that isolates stator compartment 6 from rotor compartments 7a and 7b, 8 is a stator core, 9 is electrical insulating paper, 10 is a coil, 11 is a frame in which the stator core 8 is fitted in position, 12 is a cooling water compartment, 13 is a cooling jacket, 14 is a frame side plate, and 15 is a lead wire.

The stator compartment 6 is filled with a thermotropic LCP composition that consists of a thermotropic LCP and a zircon flour as indicated in Example 1 of the present invention, and the rotor compartments 7a and 7b are either

vacuum or filled with a fluid (gas or liquid).

The thermotropic LCP composition of the present invention has high insulating, heat conducting, heat expansion and reliability characteristics. If this composition is used as an electrical insulator to make an electrically insulated housing of a stator for electric machines or appliances, a resin molded stator can be produced that is not only rugged and satisfactory in adhesion but which also insures good thermal stability and electrically insulating property.

## Claims

1. A thermotropic liquid crystal polymer composition comprising at least 10 wt.% of a thermotropic liquid crystal polymer resin and from 90 wt.% to more than 85 wt.% of zircon ( $\text{ZrSiO}_4$ ), wherein said thermotropic liquid crystal polymer is a copolymer of terephthalic acid and p,p'-biphenol with a heat distortion temperature (HDT) or deflection temperature under load of 275-350°C, a copolymer chiefly composed of 2-oxy-6-naphtic acid and containing parahydroxybenzoic acid with a HDT of 180-240°C or a copolymer of parahydroxybenzoic acid and polyethylene terephthalate with a HDT of 64-210°C.
2. A method for preparing a thermotropic liquid crystal polymer composition for injection molding comprising mixing at least 10 wt.-% of a thermotropic liquid crystal polymer resin with from 90 wt.-% to more than 85 wt.-% of zircon comprising particles of 1-60  $\mu\text{m}$  in size while heating at a temperature of 260-330°C, wherein said thermotropic liquid crystal polymer is a copolymer of terephthalic acid and p,p'-biphenol with a heat distortion temperature (HDT) or deflection temperature under load of 275-350°C, a copolymer chiefly composed of 2-oxy-6-naphtic acid and containing parahydroxybenzoic acid with a HDT of 180-240°C or a copolymer of parahydroxybenzoic acid and polyethylene terephthalate with a HDT of 64-210°C.
3. An electrical insulator having at least 10 wt.-% of a thermotropic liquid-crystalline polymer resin filled with from 90 wt.-% to more than 85 wt.-% of zircon ( $\text{ZrSiO}_4$ ) comprising particles of 1-60  $\mu\text{m}$  in size, wherein said thermotropic liquid crystal polymer is a copolymer of terephthalic acid and p,p'-biphenol with a heat distortion temperature (HDT) or deflection temperature under load of 275-350°C, a copolymer chiefly composed of 2-oxy-6-naphtic acid and containing parahydroxybenzoic acid with a HDT of 180-240°C or a copolymer of parahydroxybenzoic acid and polyethylene terephthalate with a HDT of 64-210°C.
4. A method for preparing an electrical insulator comprising the steps of:
 

first mixing at least 10 wt.-% of a thermotropic polymer resin with from 90 wt.-% to more than 85 wt.-% of zircon comprising particles of 1-60  $\mu\text{m}$  in size while heating at a temperature of 260-330 °C to form pellets having a homogeneous thermotropic polymer composition, wherein said thermotropic liquid crystal polymer is a copolymer of terephthalic acid and p,p'-biphenol with a heat distortion temperature (HDT) or deflection temperature under load of 275-350°C, a copolymer chiefly composed of 2-oxy-6-naphtic acid and containing parahydroxybenzoic acid with a HDT of 180-240°C or a copolymer of parahydroxybenzoic acid and polyethylene terephthalate with a HDT of 64-210°C, and thereafter performing injection molding with the pellets at a temperature of 260-330 °C under a pressure of 39.24 - 137.34 MPa (400 - 1,400 kgf/cm<sup>2</sup>).
5. A resin molded stator for electric machines or appliances that has an insulated housing formed by the injection molding, using the electrical insulator of claim 3, of a coil with or without iron core for electric machines or appliances and the entire part of the stator inclusive of said coil and terminals thereof.
6. A method for preparing a resin molded stator of a submersible motor comprising the steps of:
 

mixing at least 10 wt.-% of a thermotropic polymer resin with from 90 wt.-% to more than 85 wt.-% of zircon comprising particles of 1-60  $\mu\text{m}$  in size while heating at a temperature of 260-330°C to form pellets comprising a homogeneous thermotropic polymer composition, wherein said thermotropic liquid crystal polymer is a copolymer of terephthalic acid and p,p'-biphenol with a heat distortion temperature (HDT) or deflection temperature under load of 275-350°C, a copolymer chiefly composed of 2-oxy-6-naphtic acid and containing parahydroxybenzoic acid with a HDT of 180-240°C or a copolymer of parahydroxybenzoic acid and polyethylene terephthalate with a HDT of 64-210°C, and performing injection molding with the pellets at a temperature of 260-330°C through two stages, the first stage in which the slots in the stator core and the space around the coil end portions at opposite ends of the core

are filled with a resin composition at a pressure of 58.86-137.34 MPa (600-1400 kgf/cm<sup>2</sup>) and the second stage in which a can, a frame and frame side plates are mounted on the thus produced stator core to form a submersible motor and the resulting space around the coil end portions is filled with a resin composition at a pressure of 39.34-68.67 MPa (400-700 kgf/cm<sup>2</sup>).

## Patentansprüche

1. Thermotrope Flüssigkristallpolymerzusammensetzung, die mindestens 10 Gew.-% eines thermotropen Flüssigkristallpolymerharzes und 90 Gew.-% bis zu mehr als 85 Gew.-% Zirkon ( $\text{ZrSiO}_4$ ) umfaßt, wobei das thermotrope Flüssigkristallpolymer ein Copolymer aus Terephthalsäure und p, p'-Biphenol mit einer Formbeständigkeitstemperatur (HDT) oder Warmfestigkeitsgrenze von 275-350°C unter Belastung, ein hauptsächlich aus 2-Oxo-6-Naphthoesäure bestehendes Copolymer, das Parahydroxybenzoesäure mit einer HDT von 180-240°C enthält, oder ein Copolymer von Parahydroxybenzoesäure und Polyethylenterephthalat mit einer HDT von 64-210°C ist.
2. Verfahren zur Herstellung einer thermotropen Flüssigkristallpolymerzusammensetzung zum Spritzgießen, mit einem Mischen von mindestens 10 Gew.-% eines thermotropen Flüssigkristallpolymerharzes mit 90 Gew.-% bis zu mehr als 85 Gew.-% Zirkon ( $\text{ZrSiO}_4$ ) mit Partikeln in der Größe von 1-60 µm, während eines Erwärms auf eine Temperatur von 260-330°C, wobei das thermotrope Flüssigkristallpolymer ein Copolymer aus Terephthalsäure und p, p'-Biphenol mit einer Formbeständigkeitstemperatur (HDT) oder Warmfestigkeitsgrenze von 275-350 °C unter Belastung, ein hauptsächlich aus 2-Oxo-6-Naphthoesäure bestehendes Copolymer, das Parahydroxybenzoesäure mit einer HDT von 180-240°C enthält, oder ein Copolymer aus Parahydroxybenzoesäure und Polyethylenterephthalat mit einer HDT von 64-210°C ist.
3. Elektrischer Isolator mit mindestens 10 Gew.-% eines thermotropen flüssigkristallinen Polymerharzes, das mit 90 Gew.-% bis zu mehr als 85 Gew.-% Zirkon ( $\text{ZrSiO}_4$ ) mit Partikeln in der Größe von 1-60 µm gefüllt ist, wobei das thermotrope Flüssigkristallpolymer ein Copolymer aus Terephthalsäure und p, p'-Biphenol mit einer Formbeständigkeitstemperatur (HDT) oder Warmfestigkeitsgrenze von 275-350°C unter Belastung, ein hauptsächlich aus 2-Oxo-6-Naphthoesäure bestehendes Copolymer, das Parahydroxybenzoesäure mit einer HDT von 180-240°C enthält, oder ein Copolymer aus Parahydroxybenzoesäure und Polyethylenterephthalat mit einer HDT von 64-210°C ist.
4. Verfahren zur Herstellung eines elektrischen Isolators, mit den Schritten:  
 zunächst einem Mischen von mindestens 10 Gew.-% eines thermotropen Polymerharzes mit 90 Gew.-% bis zu mehr als 85 Gew.-% Zirkon ( $\text{ZrSiO}_4$ ) mit Partikeln in der Größe von 1-60 µm, während eines Erwärms auf eine Temperatur von 260-330°C zum Ausbilden von Kügelchen mit einer homogenen thermotropen Polymerzusammensetzung, wobei das thermotrope Flüssigkristallpolymer ein Copolymer aus Terephthalsäure und p, p'-Biphenol mit einer Formbeständigkeitstemperatur (HDT) oder Warmfestigkeitsgrenze von 275-350°C unter Belastung, ein hauptsächlich aus 2-Oxo-6-Naphthoesäure bestehendes Copolymer, das Parahydroxybenzoesäure mit einer HDT von 180-240°C enthält, oder ein Copolymer aus Parahydroxybenzoesäure und Polyethylenterephthalat mit einer HDT von 64-210°C ist, und  
 danach einem Durchführen des Spritzgießens mit den Kügelchen bei einer Temperatur von 260-330°C unter einem Druck von 39,24-137,34 MPa (400-1400 kgf/cm<sup>2</sup>).
5. Harzgeformter Stator für elektrische Maschinen oder Geräte mit einem isolierten Gehäuse, das durch das Spritzgießen von einer Wicklung mit oder ohne Eisenkern für elektrische Maschinen oder Geräte und des gesamten Teils des Stators einschließlich der Wicklung und ihrer Anschlüsse ausgebildet ist, wobei der elektrische Isolator von Anspruch 3 verwendet wird.
6. Verfahren zur Herstellung eines harzgeformten Stators eines Tauchmotors, mit den Schritten:  
 einem Mischen von mindestens 10 Gew.-% eines thermotropen Polymerharzes mit 90 Gew.-% bis zu mehr als 85 Gew.-% Zirkon ( $\text{ZrSiO}_4$ ) mit Partikeln in der Größe von 1-60 µm, während eines Erwärms auf eine Temperatur von 260-330°C zum Ausbilden von Kügelchen mit einer homogenen thermotropen Polymerzusammensetzung,  
 wobei das thermotrope Flüssigkristallpolymer ein Copolymer aus Terephthalsäure und p, p'-Biphenol mit einer



Formbeständigkeitstemperatur (HDT) oder Wärmefestigkeitsgrenze von 275-350 °C unter Belastung, ein hauptsächlich aus 2-Oxo-6-Naphthoesäure bestehendes Copolymer, das Parahydroxybenzoesäure mit einer HDT von 180-240°C enthält, oder ein Copolymer aus Parahydroxybenzoesäure und Polyethylenterephthalat mit einer HDT von 64-210°C ist, und

einem Durchführen des Spritzgießens mit den Kügelchen bei einer Temperatur von 260-330°C in zwei Stufen, einer ersten Stufe, bei der die Wicklungsschlitze in dem Stator Kern und der Raum rund um die Wicklungsendabschnitte an entgegengesetzten Enden des Stators mit einer Harzzusammensetzung bei einem Druck von 58,86-137,34 MPa (600-1400 kgf/cm<sup>2</sup>) gefüllt werden, und einer zweiten Stufe, bei der eine Hülle, ein Rahmen und Rahmenseitenplatten auf den derart erzeugten Stator Kern montiert werden, um einen Tauchmotor auszubilden, und der resultierende Raum rund um die Wicklungsendabschnitte mit einer Harzzusammensetzung bei einem Druck von 39,34-68,67 MPa (400-700 kgf/cm<sup>2</sup>) gefüllt wird.

## Revendications

1. Une composition de polymère thermotrope cristal liquide comprenant au moins 10% en masse d'une résine de polymère thermotrope cristal liquide et 90 % en masse à plus de 85 % en masse de zircon (ZrSiO<sub>4</sub>), dans laquelle ledit polymère thermotrope cristal liquide est un copolymère d'acide téréphtalique et de p,p'-bisphénol présentant une température de résistance à la chaleur (HDT) ou une température de déviation en charge comprise entre 275 et 350°C, un copolymère principalement composé d'acide 2-oxy-6-naphtoïque et contenant de l'acide parahydroxybenzoïque présentant une HDT comprise entre 180 et 240°C, ou un copolymère d'acide parahydroxybenzoïque et de téréphtalate de polyéthylène présentant une HDT comprise entre 64 et 210 °C.
2. Un procédé de préparation d'une composition de polymère thermotrope cristal liquide pour moulage par injection, comprenant les étapes consistant à mélanger au moins 10 % en masse d'une résine de polymère thermotrope cristal liquide avec 90 % en masse à plus de 85 % en masse de zircon comprenant des particules présentant une taille comprise entre 1 et 60 µm, tout en chauffant à une température comprise entre 260 et 330 °C, dans lequel ledit polymère thermotrope cristal liquide est un copolymère d'acide téréphtalique et de p,p'-bisphénol présentant une température de résistance à la chaleur (HDT) ou une température de déviation en charge comprise entre 275 et 350°C, un copolymère principalement composé d'acide 2-oxy-6-naphtoïque et contenant de l'acide parahydroxybenzoïque présentant une HDT comprise entre 180 et 240°C, ou un copolymère d'acide parahydroxybenzoïque et de téréphtalate de polyéthylène présentant une HDT comprise entre 64 et 210 °C.
3. Un isolant électrique comprenant au moins 10 % en masse d'une résine de polymère thermotrope cristal liquide chargée avec 90 % en masse à plus de 85 % en masse de zircon (ZrSiO<sub>4</sub>) comprenant des particules présentant une taille comprise entre 1 et 60 µm, dans lequel ledit polymère thermotrope cristal liquide est un copolymère d'acide téréphtalique et de p,p'-bisphénol présentant une température de résistance à la chaleur (HDT) ou une température de déviation en charge comprise entre 275 et 350°C, un copolymère principalement composé d'acide 2-oxy-6-naphtoïque et contenant de l'acide parahydroxybenzoïque présentant une HDT comprise entre 180 et 240°C, ou un copolymère d'acide parahydroxybenzoïque et de téréphtalate de polyéthylène présentant une HDT comprise entre 64 et 210 °C.
4. Un procédé de préparation d'un isolant électrique comprenant les étapes consistant à :
  - commencer par mélanger au moins 10% en masse d'une résine de polymère thermotrope avec 90 % en masse à plus de 85 % en masse de zircon comportant des particules dont la taille est comprise entre 1 et 60 µm, tout en chauffant à une température comprise entre 260 et 330°C pour former des pastilles présentant une composition de polymère thermotrope homogène,
  - dans lequel ledit polymère thermotrope cristal liquide est un copolymère d'acide téréphtalique et de p,p'-bisphénol présentant une température de résistance à la chaleur (HDT) ou une température de déviation en charge comprise entre 275 et 350°C, un copolymère principalement composé d'acide 2-oxy-6-naphtoïque et contenant de l'acide parahydroxybenzoïque présentant une HDT comprise entre 180 et 240°C, ou un copolymère d'acide parahydroxybenzoïque et de téréphtalate de polyéthylène présentant une HDT comprise entre 64 et 210 °C, puis à
  - réaliser ensuite un moulage par injection avec les pastilles, à une température comprise entre 260 et 330°C et sous une pression comprise entre 39,24 et 137,34 MPa (entre 400 et 1 400 kgf/cm<sup>2</sup>).
5. Un stator en résine moulée pour des machines ou appareils électriques présentant un boîtier isolant, formé par

le moulage par injection, en utilisant l'isolant électrique de la revendication 3, d'une bobine avec ou sans noyau de fer pour machines ou appareils électriques, et de toute la partie du stator, y compris ladite bobine et ses bornes.

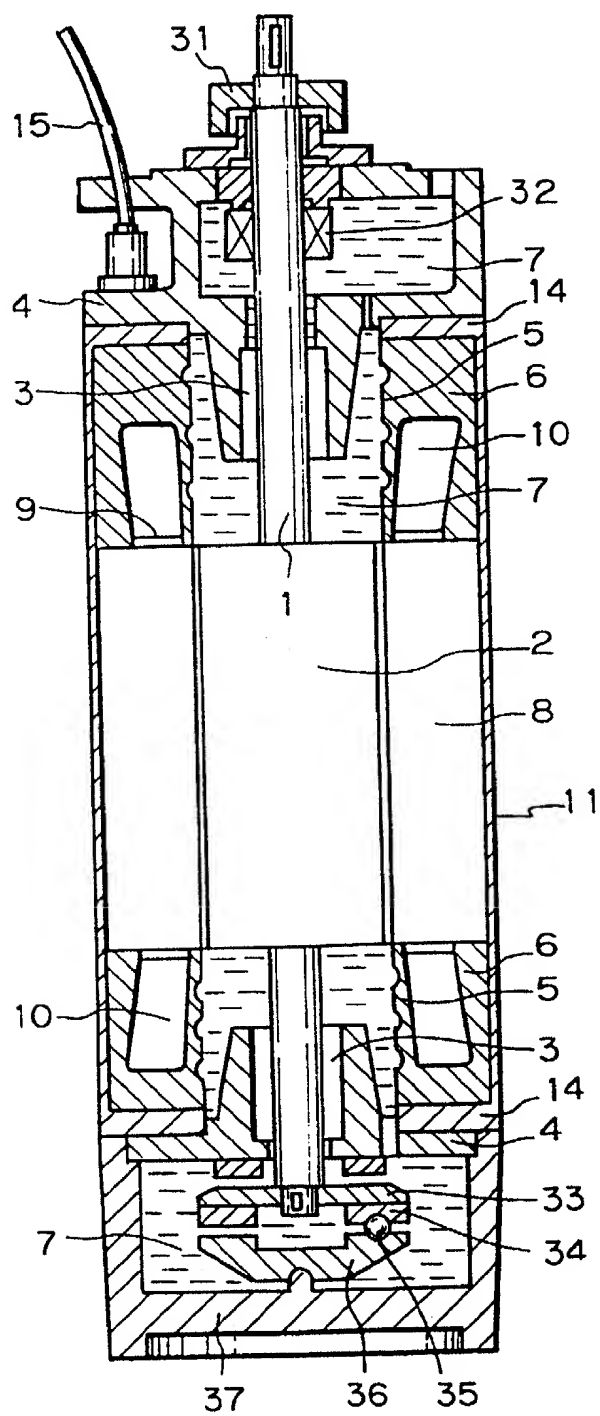
- 5 6. Un procédé de préparation d'un stator en résine moulée d'un moteur submersible, comprenant les étapes consistant à :

10 mélanger au moins 10 % en masse d'une résine de polymère thermotrope avec 90 % en masse à plus de 85 % en masse de zircon comportant des particules dont la taille est comprise entre 1 et 60  $\mu\text{m}$ , tout en chauffant à une température comprise entre 260 et 330 °C pour former des pastilles présentant une composition de polymère thermotrope homogène,

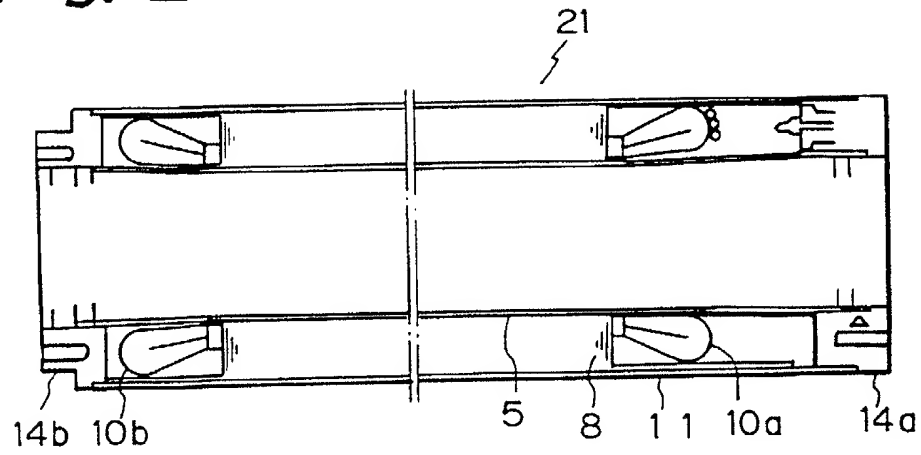
15 dans lequel ledit polymère thermotrope cristal liquide est un copolymère d'acide téréphtalique et de p,p'-bis-phénol présentant une température de résistance à la chaleur (HDT) ou une température de déviation en charge comprise entre 275 et 350°C, un copolymère principalement composé d'acide 2-oxy-6-naphtoïque et contenant de l'acide parahydroxybenzoïque présentant une HDT comprise entre 180 et 240°C, ou un copolymère d'acide parahydroxybenzoïque et de téréphtalate de polyéthylène présentant une HDT comprise entre 64 et 210 °C, puis à

20 réaliser ensuite un moulage par injection avec les pastilles, à une température comprise entre 260 et 330°C, en procédant en deux étapes, la première étape dans laquelle les encoches du noyau du stator et l'espace entourant les portions d'extrémité de la bobine aux extrémités opposées du noyau sont chargés d'une composition de résine à une pression comprise entre 58,86 et 137,34 MPa (entre 6000 et 1 400 kgf/cm<sup>2</sup>), et la seconde étape dans laquelle un boîtier, un châssis et des plaques latérales de châssis sont montés sur le noyau du stator ainsi produit pour former un moteur submersible, l'espace obtenu autour des portions d'ex-  
25 trémité de la bobine étant chargé d'une composition de résine à une pression comprise entre 39,34 et 68,67 MPa (entre 400 et 700 kgf/cm<sup>2</sup>).

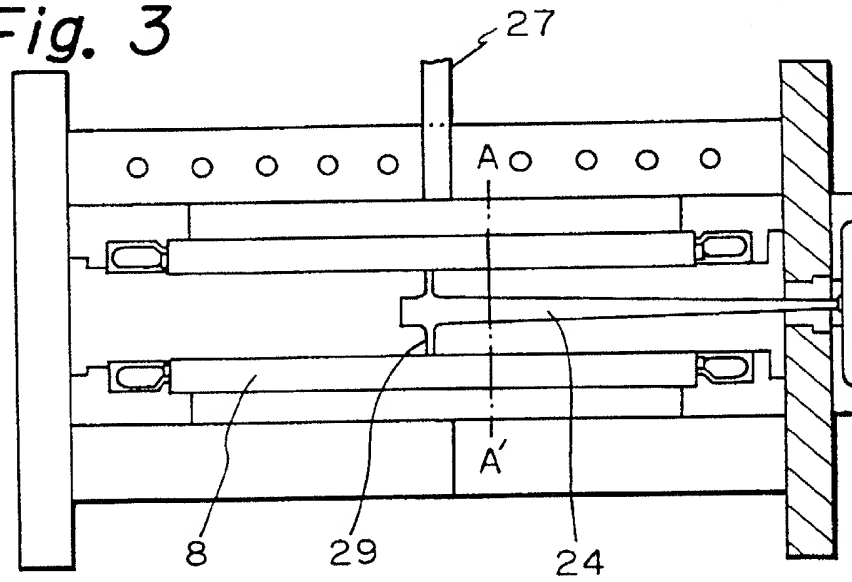
*Fig. 1*



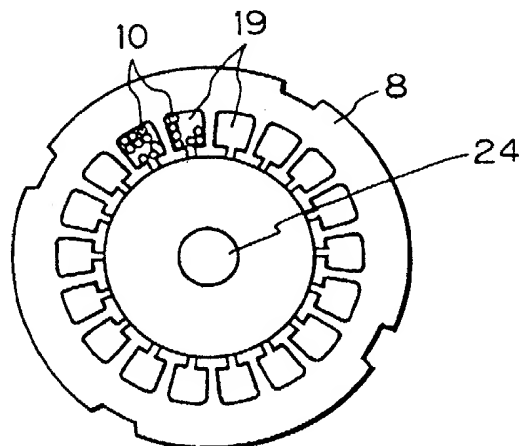
*Fig. 2*



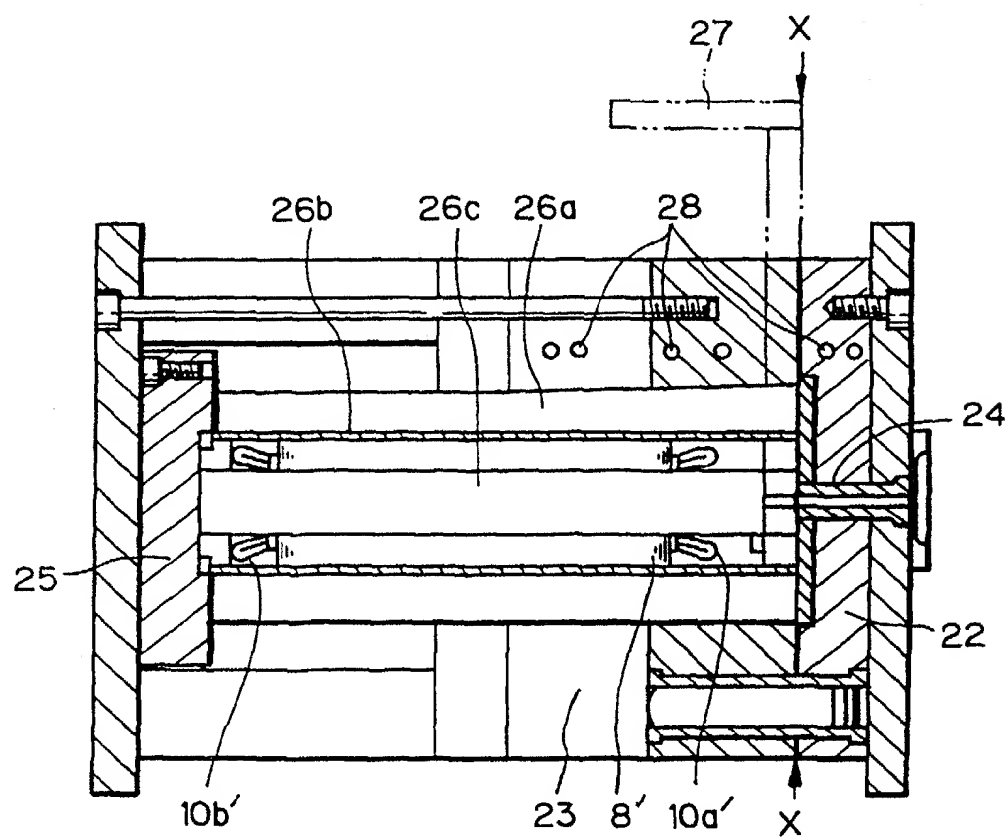
*Fig. 3*



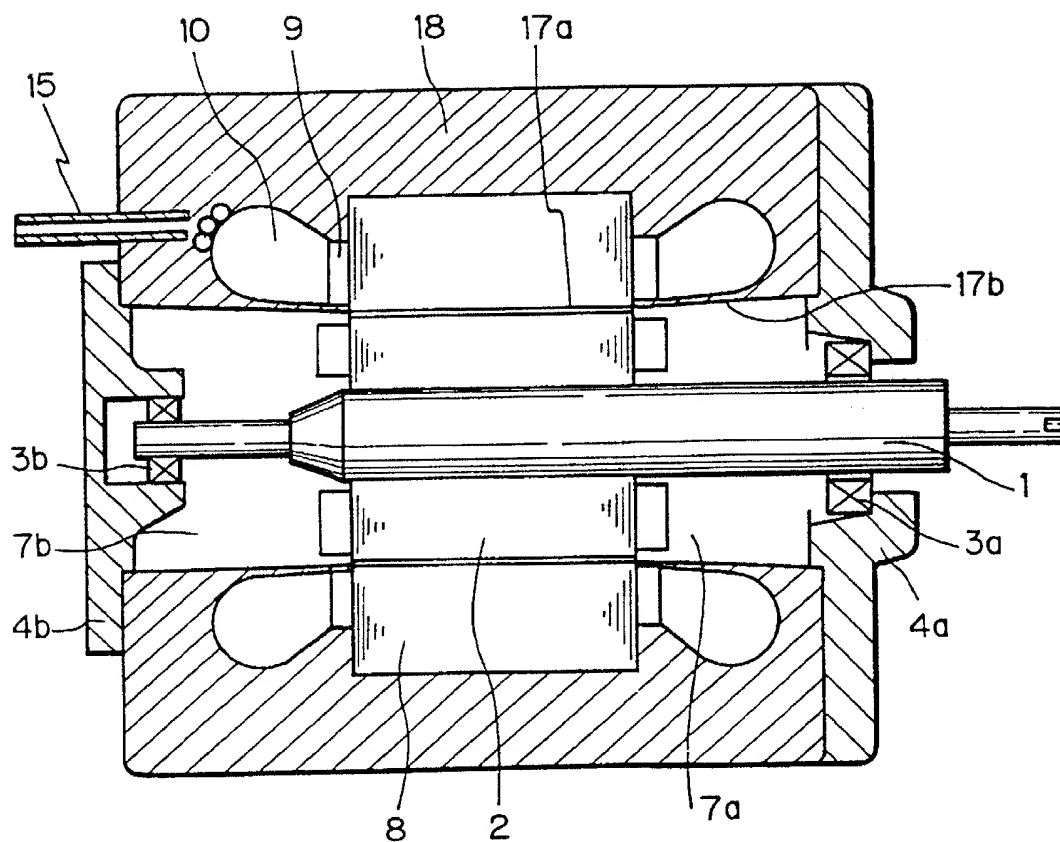
*Fig. 4*



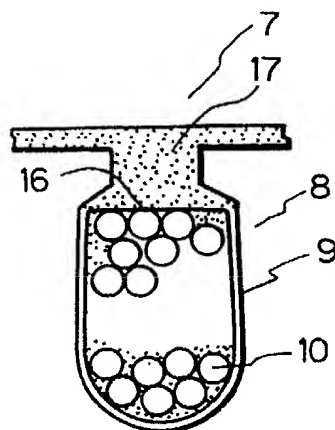
*Fig. 5*



*Fig. 6*



*Fig. 7*



*Fig. 8*

